#### **Structured Electronic Design**

#### EE3C11 Design of low-noise feedback amplifier configurations

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The equivalent input noise sources of a nonenergic feedback amplifier are equal to those of its controller



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Use an alternative method:

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 $V_{ns}$ 

 $Z_s$ 



$$S_{V_{\text{out}}} = 4kT \operatorname{Re}(Z_s) \left(\frac{R_1 + R_2}{R_2}\right)^2$$

$$S_{V_s} = 4kT \operatorname{Re}(Z_s)$$



 $Z_s$ 

Contribution of: $V_{eq}$ Source spectral density: $S_{V_{eq}}$ Voltage transfer to output: $\frac{R_1 + R_2}{R_2}$ 

$$S_{V_{\text{out}}} = 4kT \text{Re}(Z_s) \left(\frac{R_1 + R_2}{R_2}\right)^2 + S_{V_{eq}} \left(\frac{R_1 + R_2}{R_2}\right)^2$$

$$S_{V_s} = 4kT \operatorname{Re}(Z_s) + S_{V_{eq}}$$



 $Z_s$ 



$$S_{V_{\text{out}}} = 4kT \operatorname{Re}(Z_s) \left(\frac{R_1 + R_2}{R_2}\right)^2 + S_{V_{eq}} \left(\frac{R_1 + R_2}{R_2}\right)^2 + S_{I_{eq}} \left(\frac{R_1 + R_2}{R_2}\right)^2 \left(Z_s + \frac{R_1 R_2}{R_1 + R_2}\right)^2$$

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 $S_{V_s} = 4kT \operatorname{Re}(Z_s) + S_{V_{eq}} + S_{I_{eq}} \left( Z_s + \frac{R_1 R_2}{R_1 + R_2} \right)^2 + 4kT \frac{R_1^2 R_2}{(R_1 + R_2)^2}$ 



 $\left(s_{s}+\frac{R_{1}R_{2}}{R_{1}+R_{2}}\right)^{2}+4kT\frac{R_{1}^{2}}{R_{2}}$ 

 $Z_s$ 



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#### Conclusion:

The influence of the feedback resistors in the passive feedback voltage amplifier can be accounted for as if their parallel connection is in series with the source.

$$S_{V_{\text{out}}} = 4kT \text{Re}(Z_s) \left(\frac{R_1 + R_2}{R_2}\right)^2 + S_{V_{eq}} \left(\frac{R_1 + R_2}{R_2}\right)^2 + S_{I_{eq}} \left(\frac{R_1 + R_2}{R_2}\right)^2 \left(Z_s + \frac{R_1 R_2}{R_1 + R_2}\right)^2 + 4kT \frac{R_1^2}{R_2} + 4kT R_1$$

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 $V_{ns}$ 

 $Z_s$ 

 $V_s$ 





Α

#### Voltage amplifier



Α

В

Voltage amplifier

#### Transadmittance







 $Z_2$ 

 $Z_{\ell}$ 





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# As if the feedback impedance





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